

$$V(t) = V_{DC} + V_0 \sin(\omega t + \phi)$$

$$\uparrow \quad \downarrow = \frac{1}{T} \int_0^T \sin(\omega t + \phi) dt$$

Sine Waveforms
 $v(t) = V_0 \sin(\omega t + \phi)$

Sine r.m.s

$$V_{rms} = \frac{V_0 - pk}{\sqrt{2}}$$

$$I_{rms} = \frac{I_0 - pk}{\sqrt{2}}$$

r.m.s value:

equivalent amplitude of
D.C.-only signal for which
resistor dissipate same power

for sine waveform
through origin $V_{DC} = 0$

sine passing through
diode True only

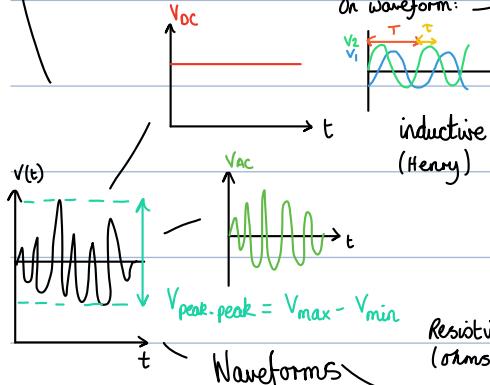
Phasors
rotating vectors



Magnitudes are V_2 and V_1 length

θ , angle between is phase difference

$$\theta = \frac{1}{T} \times 2\pi$$



On waveform:
 V_2/V_1 True only

inductive (Henry)

capacitive (Farad)

resistive (ohms)

Waveforms

$$V(t) = V_{DC} + V_{AC}$$

Mean value (\bar{V})

$$= \frac{1}{t_2 - t_1} \int_{t_1}^{t_2} V(t) dt$$

Never perfect reflection of associated quantities
→ noise, interference and distortion

Small signals → insufficient power
drive actuators

Interpretation

Display

Actuation

Processing - Amplification

Storage

Filtering

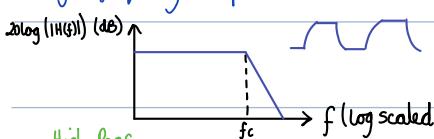
described by transfer function
 $H(f) = \frac{V_{out}(f)}{V_{in}(f)}$ in freq. domain

$$\text{or } |H(f)| (\text{dB}) = 20 \log_{10} \left(\frac{|V_{out}(f)|}{|V_{in}(f)|} \right)$$

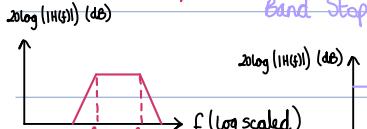
dB scaled gives straight line approximations

Low Pass - lets low pass

- Attenuates and phase shifts higher frequency components



Band Pass - allows band of freq.



Band Stop



$$V_{rms} = \frac{V_0 - pk}{\sqrt{2}}$$

$$I_{rms} = \frac{I_0 - pk}{\sqrt{2}}$$

Slew Rate

$$\max \left(\left| \frac{dv}{dt} \right| \right)$$

→ gradient of
V-t waveform

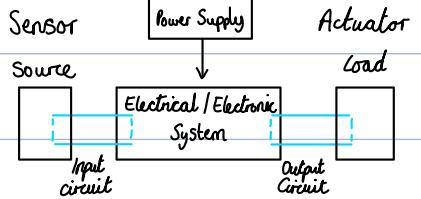
Square wave $\approx \infty$

for non-periodic waveform:

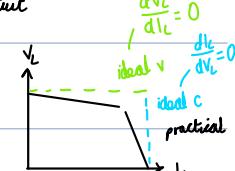
period / frequency doesn't apply

→ slew rate can still be defined

→ not found mathematically, only by observing signal for long time.



Complete System



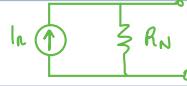
Application of load doesn't change values

Ideal Voltage Source:
- Zero resistance
→ all voltage dropped across circuit

Series, voltage source

Ideal Current Source:
- infinite resistance
→ doesn't react to applied voltage

Parallel, current source



Method:

- R_{th} : zero all sources and calculate equivalent total resistance

$$\text{Voltage Source} = \text{short} \quad (\text{as } V_{R_{th}} = 0)$$

$$\text{Current Source} = \text{open} \quad (\text{as } I_{R_{th}} = \infty)$$

- $V_{th} = V_{OC}$ → remove load and calculate voltage across open output

- $I_{th} = I_{SC}$ → short output and calculate I through short

Inverting amp

- Changes polarity

- Controllable input A

- ve feedback forces $V_- = V_+$

↳ maintains $V_- = 0V$

↳ virtual earth amplifier

Non-Inverting amp

$$V_- = V_+ = V_i$$

↳ determined by R_1 and potential divider formed by R_1 and R_2

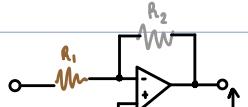
$$V_- = V_i = V_o \frac{R_1 + R_2}{R_1}$$

$$G_v = \frac{V_o}{V_i} \rightarrow G_v = 1 + \frac{R_2}{R_1}$$

- Currents I_1 and I_2 equal and opposite

$$\frac{V_o}{R_2} = - \frac{V_i}{R_1}$$

$$G_v = - \frac{R_2}{R_1}$$



Unity Gain Buffer

(like V_+ follower / V_+ buffer)

- Non-inverting

- Gain = 1

↳ buffer

- Extreme of non-inverting
where $R_2 = 0$, $R_1 = \infty$

$$V_- = V_i = V_o \frac{R_1 + R_2}{R_1}$$

$$G_v = \frac{V_o}{V_i} \rightarrow G_v = 1 + \frac{R_2}{R_1}$$

Cascading Amps

- Amps in series:

$$A = A_1 \times A_2 \times A_3$$

$$A(\text{dB}) = A_1(\text{dB}) + A_2(\text{dB}) + \dots$$

increases amp.

$$V_o = (V_2 - V_1) \frac{R_3}{R_1}$$

Clipping: limits max range of signal

→ e.g.

$$G_v = \frac{V_o}{V_i} \rightarrow G_v = 1 + \frac{R_2}{R_1}$$

$$V_o = (V_2 - V_1) \frac{R_3}{R_1}$$

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